

INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification⁶:

C06B 29/02

A1

(11) International Publication Number:

WO 98/18742

(43) International Publication Date:

7 May 1998 (07.05.98)

(21) International Application Number: PCT/US97/17329

(22) International Filing Date: 26 September 1997 (26.09.97)

(30) Priority Data:

741,247

30 October 1996 (30.10.96)

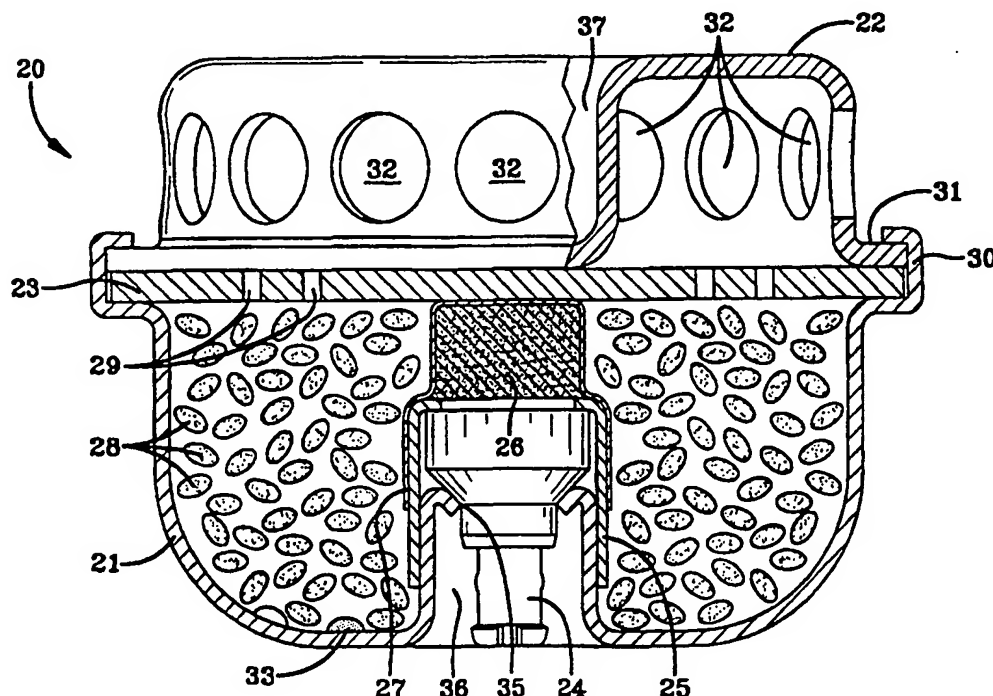
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BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC,
NL, PT, SE).

Published

*With international search report.**Before the expiration of the time limit for amending the
claims and to be republished in the event of the receipt of
amendments.*

(54) Title: AUTOIGNITION COMPOSITION FOR AN AIRBAG INFLATOR



(57) Abstract

An autoigniting composition (33) contains lead thiocyanate $Pb(SCN)_2$ as the fuel, a chlorate as the oxidizer and optionally, a binder and/or a flow agent/thickener is employed in an inflator (20) used to inflate a vehicle occupant restraint such as an airbag. The autoignition composition undergoes rapid autoignition at temperatures from approximately 190 to 220 °C and consequently ignites a gas generating composition (28) in the inflator.

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AUTOIGNITION COMPOSITION FOR AN AIRBAG INFLATOR

FIELD OF THE INVENTION

The present invention relates generally to gas generators used to inflate devices such as vehicle occupant restraints (commonly known as airbags) and more specifically to autoignition compositions that are useful in airbag systems. More particularly the present invention relates to the use of lead thiocyanate and chlorate oxidizers which provide excellent thermal stability and reliably autoignites at the desired temperature of 190-220°C. The autoignition composition of the invention also includes at least one additional element selected from binders and flow agent/thickeners.

There are a variety of devices, such as thermostats, fuses and the like, which respond to an increase in temperature beyond a specific point. Two temperature responsive devices, which are employed in inflatable restraint systems, (hereinafter referred to as "airbags"), are igniters and thermal batteries. These temperature responsive devices are used to intentionally activate the airbag system when it is exposed to an unusually high temperature, such as in a fire. The inclusion of an autoignition material in an inflator assembly incurs increased expense as the autoignition material must be carefully prepared, handled and installed. Also, the temperature sensitivity of the autoignition material should not vary over the lifetime of the vehicle in which it is installed.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention, both as to its structure and manner of operation, may best be understood by
5 referring to the following detailed description, taken in accordance with the accompanying drawings in which:

Fig. 1 is a diagrammatic representation of an exemplary fluid dispensing apparatus which may be used in automated production of the autoignition system of
10 the present invention;

Fig. 2 is a side view, partially in section, of an airbag inflating device which may be used with the autoignition system of the present invention;

Fig. 3 is an enlarged fragmentary view of an
15 alternative embodiment of the autoignition system of the present invention;

Fig. 4 is an enlarged fragmentary view of another alternative embodiment of the autoignition system of the present invention; and

20 Fig. 5 is an enlarged fragmentary view of another alternative embodiment of the autoignition system of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

As used herein and in the claims, the term "autoignition material" or "autoignition composition" means a material which will spontaneously ignite or combust at a lower temperature than the temperature at which the gas generating material ignites, which would lead to the catastrophic destruction (explosion, fragmentation, or rupture) of the airbag system. When the autoignition material spontaneously ignites, the generated heat ignites the gas generating material. Thus, the gas generating material is ignited at a preselected temperature, which is higher than normally encountered ambient temperatures, but lower than the temperature at which the gas generating material itself would autoignite and cause catastrophic destruction.

Basic requirements of an autoignition composition for a gas generator used in a vehicle occupant restraint system are that the autoignition composition be (1) thermally stable up to 110°C; (2) not autoignite below 150°C; (3) autoignite rapidly at approximately 190-220°C; and (4) possess physical integrity to withstand abrasion and environmental changes. Vehicle occupant restraint inflator systems must pass aging requirements in order to assure reliable ignition despite exposure to a wide range of temperatures over the life of a vehicle.

In operation, the relatively low autoignition temperatures, i.e., approximately 190-220°C, characteristic of the composition of the present invention are maintained following long-term high temperature aging, for example, after 400 hours at 107°C. The autoignition compositions of the present

invention therefore ensure ignition reliability despite exposure to a wide range of temperatures over the life of the vehicle, which may be ten (10) or more years.

5 In operation, the autoignition composition of this invention will produce enough heat to raise the gas generating material to its ignition temperature. Since the autoignition composition is not packaged in a separate container, as in most of the prior art, the
10 autoignition composition of the present invention will effectively and reliably ignite the gas generant. In one embodiment of this invention, the autoignition globule may be in the proximity of an additional ignition material. For example, small pellets or
15 granules of a common ignition material such as BKNO_3 can be utilized as a booster.

 The housing for an airbag inflation device according to the present invention can be made of metal, steel, aluminum, aluminum alloys, stainless
20 steel and the like. While the housings employed are commonly metal and preferably aluminum, it is understood that the present invention could be employed with a housing made of plastic, ceramic or any other suitable material.

25 Those skilled in the art will understand how $\text{Pb}(\text{SCN})_2$ and chlorate oxidizers can be combined to form an autoignition composition that ignites at temperatures from 190-220°C. Most preferably, the autoignition composition of the present invention will
30 have an autoignition temperature of about 190-210°C. The weight ratio of $\text{Pb}(\text{SCN})_2$ to chlorate oxidizer can be from 3:1 to 1:3. Preferably, the ratio is in the range of 2:1 to 1:2 with the most preferred ratio being 1:1. On a weight % basis, the lead thiocyanate

can range from 25-50% and the chlorate oxidizer can range from 25-50%. The weight percent ranges for the paste, slurry or paint are 15-40% for each of the fuel and oxidizer.

5 The preferred components of the autoignition system of the present invention are lead thiocyanate ($\text{Pb}(\text{SCN})_2$) and potassium chlorate (KClO_3) at a 1:1 weight ratio. $\text{Pb}(\text{SCN})_2$ is incompatible with aluminum as it causes corrosion of the aluminum. Corrosion of
10 the aluminum housing is highly undesirable and must be prevented. It has been found that an autoignition material containing $\text{Pb}(\text{SCN})_2$ and a chlorate oxidizer can be applied to an interior surface of an aluminum inflator housing without causing corrosion, provided a
15 barrier is applied to the surface of the aluminum prior to the application of the autoignition composition.

 The barrier material for use with aluminum housings can be any conventional paint or substance
20 that will adhere to aluminum, be resistant to thermal degradation to the upper extreme of the required storage temperature (about 107°C for a period of 400 hours minimum), be non-porous to the autoignition composition, suitable for automated dispensing, and
25 allow for adherence of the autoignition composition. Representative of useful barrier materials are acrylates and silicones. A preferred barrier material is Loctite® 3201 Ultraviolet Curable Urethane Acrylate Resin sold by the Loctite Corporation of Rocky Hill,
30 Connecticut. The same material used for the barrier may also be used to coat the autoignition globule to prevent absorption of water into the globule and to provide protection from abrasion caused by pellets or granules of the gas generating composition.

It has been found useful to combine the $\text{Pb}(\text{SCN})_2$ and chlorate oxidizer with binders to promote the formation of an adherent and cohesive globule. Known solvent based and water based binders such as hydrated
5 lime ($\text{Ca}(\text{OH})_2$), sodium silicate (NaSiO), carboxymethylcellulose, natural rubber, synthetic rubber, synthetic resins and the like, can be used. Representative of the solvent based cements, resins or lacquers that are useful in the present invention as
10 binders include ethylcellulose, polyamides, polyurethanes and epoxy compounds. The binder is preferably water soluble, and enhances the adhesive properties of the $\text{Pb}(\text{SCN})_2$ and oxidizer mixture. Representative of the water based binders that can be
15 used in the present invention include starch, dextrans, gums, albumin, sodium silicate, sodium carboxymethylcellulose, lignin and polyvinyl alcohol (PVA). There is also a class of binders that may be used in the invention and they are known as the
20 water/solvent based binders. Representative of such materials are the resin esters, resorcinol formaldehyde, phenol formaldehyde, polyvinyl ethers and the like. Representative of preferred binders include Cerama-Bind 642, 643 and 644 sold by Aremco
25 Products of Ossining, New York which are water soluble inorganic silicates and the Elvanol® brand of polyvinyl alcohols (PVA) sold by du Pont. Of the series of Elvanol® hydrolyzed polyvinyl alcohol binders, Elvanol® 52-22 is preferred. Also useful as binders in the
30 present invention are a class of materials known as the sodium silicates. The ratio of silica (SiO_2) to sodium oxide (Na_2O) can be varied to meet the requirements of a wide range of end uses. A number of sodium silicates sold by Power Silicates, Inc. of

Augusta, Georgia U.S.A. have been found to be useful in the present invention. Combinations of various binders are contemplated for use in the autoignition compositions of the present invention.

5 The weight ratio of the binder material to the sum of the $\text{Pb}(\text{SCN})_2$ and the chlorate oxidizer can range from 1:100 to 1:1. A more preferred range is 1:50 to 1:1 with the most preferred ratio being 3:97. On a weight % basis, the binder is present in the
10 composition at from 0-5%. The binder material should not react with the other components of the autoignition composition prior to autoignition and should result in a smooth texture for the paste or paint. After drying, the autoignition composition
15 with binders should be one continuous mass having a hard, smooth, tough surface. The most preferred binder is Cerama-Bind, Grade 642, which also is useful as a coating material for the globule.

 The use of flow agents/thickeners are also
20 beneficial to the autoignition composition of this invention, as they promote the formation of pastes or paints which can be applied to the interior of the inflator housing through automated dispensing devices. Those skilled in the art will appreciate that any
25 known flow agent and/or thickener will be useful in the present invention provided that it does not react with the other components of the composition prior to ignition and is compatible with the solvent (water, organic or mixtures) used to prepare the reactive
30 slurry. If the autoignition composition is solvent based, the flow agent/thickener should be hydrophobic and hydrophilic when water based. The use of materials such as hydrophilic silica and talc to enhance the wetting characteristics of the composition

have been found to be useful for aqueous based compositions. A preferred hydrophilic flow agent/thickener is Aerosil® 300 which is distributed by Degussa Corporation. Aerosil® 300 is a hydrophilic silica having a high specific surface area which provides an enhanced thickening and thixotropic effect. Other hydrophilic silicas that have been found useful in the present invention include Cab-O-Sil® M5 from Cabot Corporation and Zeotaix® 265 from the J.M. Huber Corporation. The weight ratio of the flow agent/thickener to the sum of the $\text{Pb}(\text{SCN})_2$ and the oxidizer can range from 1:100 to 1:1. A more preferred range is 1:50 to 1:1 with the most preferred ratio being 3:97. On a weight % basis, the flow agent/thickener is present at from 0-5%.

One novel aspect of the autoignition composition according to this invention is that the composition may be formulated and applied as a paint or paste. The paste is formed by mixing the dry components with a liquid such as water, organic solvents and mixtures thereof. The amount of liquid can range from 10-40% by weight of the composition, with 20-30% by weight being more preferred.

As used herein, the terms "slow hot plate test" or "slow heat ignition test" mean a test wherein samples of the autoignition material are placed in an aluminum pan and dried. The pan, with samples, is then placed on a cool hot plate and the hot plate is then turned on and set on "high". The hot plate has an attached thermocouple to record temperatures. The temperature at zero time is noted and then recorded every five (5) minutes as the temperature rises. While heating the test samples, they were observed for

discoloration, exudation, burning, explosion and the like. Typically, the rate of heating is about 5-10°C/minute. This test is a very rigorous test for autoignition compositions since, under such

5 conditions, many compositions slowly decompose under the increasing temperatures and thereby fail to ignite at the desired temperature, for example, 190-220°C.

EXAMPLE I

10

The autoignition compositions in accordance with a preferred embodiment of this invention comprise $\text{Pb}(\text{SCN})_2$ as the fuel, a chlorate oxidizer, a water soluble binder and a hydrophilic flow agent/thickener.

15 The mixing of the compositions can be accomplished through the use of known equipment in the art. In this Example, lead thiocyanate, potassium chlorate and Aerosil® 300 (hydrophilic silica) were added to a dry blender with velostat chips and mixed for 30 minutes.

20 An aqueous solution of Elvanol® 52-22 (PVA binder) was then added to the dry mix and blended with a wooded spatula until a smooth paste resulted. Additional water may be added to result in a desired consistency. The autoignition paste was then applied to an aluminum

25 pan as a small globule and dried in an oven at 95°C for about 1 hour. The drying of the autoignition globules may, in general, be conducted from room temperature up to about 110°C.

The precise composition of the autoignition paste

30 and the dried autoignition globule are set forth in Table 1.

TABLE 1

5	Material	% by Weight	
		Wet (paste)	Dry
	Lead Thiocynate	32.8	48.3
	Potassium chlorate	32.8	48.3
10	Aerosil 300	0.4	0.6
	Elvanol 52-22 (binder)	1.9	2.8
	Water	32.1	---

15 The globule of the dried autoignition material in the aluminum test pan (.9 mm thick, 6.35 cm in diameter and 1.25 cm deep) was then subjected to the slow heat ignition test. The temperature was increased at a rate of 5-10°C/minute. The temperature at which the composition autoignited was determined to be
20 between 190-200°C.

EXAMPLE II

25 In this example, the autoignition composition was prepared and then placed within a steel inflator housing. The potassium chlorate, lead thiocyanate and Aerosil® 300 were blended in a dry state and then a 7.73% by weight water solution of Elvanol 52-22 was added to prepare the paste. The following Table 2
30 sets forth the components of the autoignition composition on a dry weight basis and as the paste.

TABLE 2

MATERIAL	WT. IN GRAMS	WET % BY WT.	DRY WT. GMS.	DRY % BY WT.
Potassium chlorate Lead	0.9951	35.5	.9951	48.3
thiocyanate Aerosil®300 Elvanol 52-22	0.9951	35.5	0.9951	48.3
	0.0100	0.4	0.0100	0.5
	0.8036	-	-	-
solution H ₂ O from	0.7415	26.5	-	-
solution Elvanol 52-22	0.0621	2.2	0.0621	3.0
TOTAL	2.8041	100.0	2.0623	100.0

Charges or globules of the autoignition composition were applied to the inflator housing by "spooning" the paste into the interior of the housings. The following Table 3 sets forth the weight of each charge in the housing after the charge was dried.

TABLE 3

	HOUSING NUMBER	CHARGE, MG
10	1	167.0
	2	179.3
	3	152.3
	4	123.5
15	5	111.6
	6	127.4
	7	224.2
	8	126.2
	9	163.6
20	10	111.5

The housings were then subjected to the slow heat test. All of the samples autoignited at a temperature of from 190-220°C.

25

EXAMPLE III**Use of NaClO₃**

In this experiment, the use of sodium chlorate (NaClO₃) as a replacement for the KClO₃ used in Example I, was evaluated. Normally NaClO₃ is not used where KClO₃ is available because NaClO₃ absorbs atmospheric moisture more readily than KClO₃. However, in a water based autoignition composition that can be applied wet to an inflator housing, NaClO₃ is useful because it is very soluble in water.

Approximately 62.9 grams of NaClO_3 was placed in a 125 ml flask with about 75 ml of deionized water. The flask was heated and agitated to aid in solubilizing the NaClO_3 . The resulting solution had a concentration of 0.493 g NaClO_3 /g of solution. A dry mix of $\text{Ca}(\text{OH})_2$, (binder), $\text{Pb}(\text{SCN})_2$ and Aerosil® 300 (hydrophilic flow/thickening agent) was prepared and sufficient NaClO_3 solution was added to completely wet the dry mix. The composition was applied to an aluminum pan and air dried for approximately 72 hours. The content of the composition on a dry weight basis is set forth in Table 4.

TABLE 4

MATERIAL	% DRY WEIGHT
$\text{Pb}(\text{SCN})_2$	34.8
NaClO_3	45.5
$\text{Ca}(\text{OH})_2$	17.9
AEROSIL® 300	1.8

20

Four samples of this composition were evaluated using the "slow hot plate test". The rate of heating was about $6.7^\circ\text{C}/\text{minute}$. The autoignition temperature of the four samples was about 238°C . From this experiment, it was concluded that NaClO_3 may be employed in the autoignition composition of this invention. The autoignition composition using NaClO_3 as the oxidizer formed a relatively sensitive charge.

30

EXAMPLE IV

In the commercial production of airbag inflation devices, the factors of cost, weight and reliability are critical. One aspect of the present invention

resides in the mechanical or automated application of the fluid (i.e., paste or paint) autoignition composition to the inside of the inflator housing. The use of such mechanical applicators reduces labor costs and allows for the consistent application of a given amount of the autoignition composition which results in reliable and predictable ignition.

Representative of equipment useful for the mechanical application of the fluid (i.e., paste or paint) autoignition composition to the inside of the inflator housing is Model EFD100XL, Fluid Dispensing System manufactured by EFD, Inc., of East Providence, Rhode Island U.S.A. An illustration of this device is presented in Figure 1. In brief, this device uses air pressure to control the dispensing of fluids or pastes from a syringe. Devices like the EFD100XL can make very consistent dots or globules of the material to be dispensed and are readily adapted to automated systems.

An autoignition composition similar to that set forth in Example 1 was prepared except that various amounts of water were used to determine the optimum water content for the automatic dispensing device. One skilled in this art will appreciate that the water content of the composition will be dictated by factors such as the size of the dispensing device, the size of the opening of the syringe, the pressure utilized and the amount of autoignition composition to be deposited. For the above recited device, a syringe opening of 0.24 cm, a pressure of 137.9 kPa, vacuum of 103.4 kPa and a pulse of 0.01 seconds results in uniform, self-leveling globules when the water content was about 27% by weight.

EXAMPLE V

Two formulations containing $\text{Ca}(\text{OH})_2$ as the binder were prepared according to the formulations in

5 Table 5.

TABLE 5

WEIGHT %

10

MATERIAL	FORMULA V A	FORMULA V B
$\text{Ca}(\text{OH})_2$	20	30
$\text{Pb}(\text{SCN})_2$	40	35
KClO_3	40	35

15

First the non-reactive combination of $\text{Ca}(\text{OH})_2$ and $\text{Pb}(\text{SCN})_2$ was produced by dry blending these materials together with velostat chips to assure the breakdown of the agglomerates of both of these materials. After
20 processing this mix, the chips were removed, the KClO_3 was added and the resultant combination was further blended. A quantity of tap water was added to the blend to result in a plastic putty like consistency that could be used for dispensing with the air
25 pressurized syringe. The autoignition compositions were deposited onto aluminum pans using the device described in Example IV.

In the slow hot plate tests, autoignition occurred at 220°C to 270°C and did not seem to be
30 dependent upon whether 20 or 30 weight % of $\text{Ca}(\text{OH})_2$ was used. $\text{Ca}(\text{OH})_2$ appeared to be relatively non-reactive with the aluminum, however severe corrosive reaction of the aluminum by the $\text{Pb}(\text{SCN})_2$ was not abated by the use $\text{Ca}(\text{OH})_2$ as the binding material.

EXAMPLE VI

While the autoignition composition of Example V had good physical characteristics and adhered well to aluminum surfaces, its autoignition characteristics were somewhat inadequate as the autoignition temperatures were higher than desired. This experiment investigated the possibility that the autoignition composition compressed into a pellet form (no water added) and dispersed throughout the gas generating material could act as the autoignition source. Three formulations, described in Table 6, were dry mixed and pressed into pellets.

15

TABLE 6

DRY WEIGHT %

	MATERIAL	FORMULA VIA	FORMULA VIB	FORMULA VIC
20	Ca(OH) ₂	20	15	10
	Pb(SCN) ₂	39	41.5	44
	KClO ₃	39	41.5	44
	Aerosil 300	2	2	2

25

Three pellets of each composition were made by pressing about 40 to 50 mg of the mixtures at about 413,700 kPa. The diameter of these pellets was about 0.5 cm. In slow hot plate tests autoignition of Formula VIA pellets occurred at 184 to 187°C. For the Formula VIB pellets the autoignition temperatures were 194°, 200° and 205°C. The Formula VIC pellets had autoignition temperatures of 188, 188 and 199°C. These autoignition temperatures were near the preferred objective of about 190-200°C.

30

Three pellets were made from Formula VIA by pressing about 40 to 50 mg of the mixtures at about 137,900 kPa (20,000 psi). The diameter of these pellets was about 0.49 cm (0.192 inches). In slow hot plate tests of these Formula VIA pellets, autoignition occurred at 194, 201 and 219°C.

It was concluded from this experiment that the $\text{Pb}(\text{SCN})_2/\text{KClO}_3$ autoignition compositions may be diluted by up to 20% by weight with $\text{Ca}(\text{OH})_2$ and, when in the consolidated form, still function at an autoignition temperature of about 200°C in the slow hot plate test.

EXAMPLE VII

This experiment, in accordance with this invention, was conducted to investigate the deposition of autoignition materials directly on an interior surface of a steel housing. The compositions evaluated are described in Table 7. Water slurries of these compositions were prepared, applied to steel plates, dried and then subjected to slow hot plate tests.

TABLE 7

	FORMULA VIIA	WEIGHT %			
		FORMULA VIIB	FORMULA VIIC	FORMULA VIID	FORMULA VIIE
Pb(SCN) ₂	44	46.7	49.7	49.7	49.7
KClO ₃	44	46.7	49.7	49.7	49.7
Ca(OH) ₂	10	--	--	--	--
Aerosil 300	2	--	0.6	0.6	0.6
Sodium Silicate	--	6.6	--	--	--
Elvanol 52-22	--	--	5.1*	3*	--

* added to the dry ingredients via an aqueous solution

The results of the slow hot plate test of Formula VIIA are presented in Table 8. The rate of heating was about 5.5°C/min.

5

TABLE 8

PLATE NO.	CHARGE WT.		TIME	TEMP. (°C)
	(GM)	(MIN:SEC)		
1	0.1211	30:16		187
2	0.1774	30:16		187
10 3	0.1324	30:16		187

The results of the slow hot plate tests of Formula VIIB are presented in TABLE 9. The rate of hearing was about 5.5°C/min. While the charge
15 functioned, it did not propagate completely. It appears that greater than about 5% by weight sodium silicate inhibits rapid propagation.

20

TABLE 9

PLATE NO.	CHARGE WT.		TIME	TEMP. (°C)
	(GM)	(MIN:SEC)		
1	0.1941	27:07		173

The results of the slow hot plate tests of
25 Formula VIIC are presented in Table 10. The rate of heating was about 5.0°C/min. All of the charges propagated completely when they initiated. The charges appeared to have both good physical
30 characteristics and to be well bonded to the steel plate.

20

TABLE 10

	PLATE NO.	CHARGE WT. (GM)	TIME (MIN:SEC)	TEMP. (°C)
5	1	0.0324	33:42	195
	2	0.0563	35:03	201
	3	0.0486	42:58	232

The results of the slow hot plate tests of
10 Formula VIID are presented in Table 11. The rate of
heating was about 6.1°C/min.

TABLE 11

	PLATE NO.	CHARGE WT. (GM)	TIME (MIN:SEC)	TEMP. (°C)
15	1	0.1033	26:44	191
	2	0.0179	29:19	204
	3	0.0233	29:07	205

20

The results of the slow hot plate tests of
Formula VIIE are presented in Table 12. The rate of
heating was about 6.1°C/min.

TABLE 12

	PLATE NO.	CHARGE WT. (GM)	TIME (MIN:SEC)	TEMP. (°C)
25	1	0.0241	28:15	202
	2	0.0332	27:13	200
30	3	0.0179	no fire	

It was concluded that a formulation containing
about 50/50 Pb(SCN)₂/KClO₃, by weight, appears capable
of functioning as an autoignition charge which
35 activates at about 200°C when applied to metal in

liquid form with or without binders and/or flow agent/thickeners.

The formulations containing $\text{Ca}(\text{OH})_2$ (Formula VIIA) and sodium silicate 20 (Formula VIIB) as binders did not function consistently. Of the binder materials tested, the polyvinyl alcohols appear to have the best binding characteristics for the $\text{Pb}(\text{SCN})_2$ based charges.

EXAMPLE VIII

Charges of the autoignition material of Formula VII D of Example VII, in the form of a water-based slurry, were applied to an inside surface of three steel housings using an artist's paint brush. After the charges were dry, several drops of Loctite 5290 were applied over each charge so that the entire charge was coated. The purpose of this coating was to protect the autoignition charges from abrasion by the gas generating material and retard absorption of water. This coating material has a low viscosity, so the coating was very thin. Three of these units were subjected to bonfire conditions, and all three autoignited.

EXAMPLE IX

The use of a fluid dispensing system to apply the autoignition material to a surface was further investigated. The equipment used was a Model EFD 100XL Fluid Dispensing System as previously described.

Initial dispensing trials were conducted using the nonreactive formulation presented in Table 13. The dry mix was prepared and water was added to render the mix a fluid or slurry which was about 27% by weight water. The slurry mix was placed in a 3 cc plastic syringe with a plastic plunger, and the

syringe was fastened to the dispensing system. No needle was used. The opening in the syringe through which the slurry was dispensed was about 0.24 cm (0.095 inches) in diameter. At 27% by weight water, the dispensing system produced uniform globules. Table 13 sets forth the composition of the premix and the slurry.

TABLE 13

10

PREMIX

% BY WEIGHT

	WEIGHT (GMS)	WET	DRY
Pb(SCN) ₂	3.0068	70.2	97.0
15 Aerosil 300	0.0936	2.2	3.0
H ₂ O	1.1815	27.6	--

A slurry was then prepared using the reactive dry blended premix composition consisting of: 49.7% wt. Pb(SCN)₂; 49.7% wt. KClO₃; and 0.6% Aerosil 300, and with an aqueous solution containing 3% PVA 52-22, by weight. The weights of materials used in the preparation of this slurry are presented in Table 14.

TABLE 14

		% BY WEIGHT		
		WEIGHT (GMS)	WET	DRY
5	Premix	3.9997	76.3	97.0
	PVA 52-22	0.1236	2.4	3.0
	H ₂ O	1.1179	21.3	--

The water content of this reactive slurry was lower than that used in the nonreactive trial (21.3 vs. 27.6%). This was done to determine the lower limit of the water content required for good dispensing of the slurry. This reactive slurry could not be extruded from the dispensing system until the dispensing pressure was increased to about 207-241 kPa. The slurry was too dry to be self leveling, and it was concluded that about 27% water content was more suitable for automated dispensing from this particular device. The charges were subjected to slow hot plate tests and autoignited at temperatures of 189 to 206°C.

EXAMPLE X

Various levels of a $\text{Ca}(\text{OH})_2$ binder were evaluated in this experiment. A dry pre-mix of 47% $\text{Pb}(\text{SCN})_2$ and 53% KClO_3 by weight was prepared. A dry blend of the pre-mix and $\text{Ca}(\text{OH})_2$ was prepared wherein either 20% or 30% by weight of the final composition was $\text{Ca}(\text{OH})_2$. The compositions were mixed with water to result in a composition having a pasty consistency. Samples were placed in a test pan and then air dried. The weight % of water ranged from 23.5 to 37.5%. After 24 hours of air drying all charges were firmly attached to the

aluminum pan, however, cracks extending completely through the charge or globule to the bottom of the globule were noted. Some pitting and perforation (corrosion) of the aluminum pans was also noted. The weights of the four samples with 20% $\text{Ca}(\text{OH})_2$ ranged from 198 mg to 580 mg. The diameter of the charges ranged from about 1.7 cm to 2.5 cm while the thickness of the charges ranged from about 0.05 cm to about 0.18 cm. After air drying for about an additional 96 hours, the samples were tested in the slow heat test. The temperature rise was about $7.4^\circ\text{C}/\text{minute}$. All samples autoignited at from $218\text{--}232^\circ\text{C}$.

An additional sample of the 20% $\text{Ca}(\text{OH})_2$ composition and the 30% $\text{Ca}(\text{OH})_2$ composition were coated with a solution of Cerama-Bond 642 (sodium silicate). The sodium silicate solution was brushed onto the globule or charge and air dried. These samples were then evaluated in the slow heat test. The rate of temperature increase was about $7.1^\circ\text{C}/\text{minute}$. The 20% $\text{Ca}(\text{OH})_2$ exploded at 246°C while the 30% sample burned rapidly at 248°C .

EXAMPLE XI

Two Binders

To the 20% $\text{Ca}(\text{OH})_2$ dry mixture prepared in Example X was added a water solution of 1 part by volume Cerama-Bond 642 to 3 parts water. Four samples were prepared, air dried and tested in the slow heat test. The temperature rise was about $7.2^\circ\text{C}/\text{minute}$. All four samples ignited at 248°C . The experiment indicates that mixtures of binders are useful in the present invention.

EXAMPLE XII**Comparative**

The use of sulfur as a fuel for a autoignition composition that would adhere to a metal inflator housing was investigated. The stoichiometric weight ratio of sulfur to NaClO_3 is 31 to 69. A saturated aqueous solution of NaClO_3 (0.493 g of NaClO_3 per g of solution) was placed in an aluminum pan. 0.31 g of sulfur was then added and the mixture stirred with a wooden spatula. Globules of the resulting mixture were then placed in four aluminum pans and dried. The charge weights ranged from 112 mg to 382 mg. Slow heat tests were conducted with a temperature rise of 6.72°C/minute. No autoignition occurred with any charge up to a temperature of 200°C.

EXAMPLE XIII**Comparative**

In this experiment, a water mixed slurry of sulfur, Ca(OH)_2 and Aerosil® 300 was combined with a NaClO_3 saturated solution. Dried globules of this mix autoignited at temperatures as low as 138°C in the slow heat test. In other testing, mixtures of sulfur, NaClO_3 , Ca(OH)_2 and sodium silicate demonstrated autoignition at storage temperatures of 95°C. It was also determined that sulfur is rapidly lost through oxidation at temperatures above 107°C. From Example XII and this example, it is clear that sulfur is not an appropriate fuel for an autoignition composition.

Detailed Description of the Drawings

Referring to Figure 1, there is shown an exemplary air powered fluid dispensing device 10 which may be used to apply the autoignition composition of the present invention to the interior of an inflator housing. The device 10 may also be used to apply the barrier material 41 of Figure 1 for the autoignition material and may also be used to apply the coating 43 of Figure 5. In general, the fluid dispensing device 10 consists of a control unit 11, a foot pedal 12, an air hose 16 and a no-drip syringe system 17. The control unit 11 contains means for an adjustable output air regulator 13 which provides control of fluid flow, means to adjust dispense time 14 and means to control barrel (syringe) vacuum 15 to facilitate the dispensing of low viscosity liquids. An air hose 16 connects the control unit 11 to the no-drip syringe system 17. Syringe system 17 is held in a storage stand 18. The foot pedal 12 is connected to the control unit 11 to provide manual fluid flow control.

Referring to Figure 2, there is shown an exemplary gas generating device 20 which may be used with the autoignition system of the present invention. This exemplary gas generating device may be employed as a component of a vehicle occupant restraint system of the type which deploys an airbag to protect a vehicle occupant in the event of a crash. When a crash sensor (not shown) detects a crash of a preselected severity it closes an electrical circuit or initiates a firing signal which activates a squib 24 which ignites a booster composition 26, which in turn ignites the gas generating composition 28 located in the housing 21. As used herein a squib is

understood to be an electrical device having two electrodes insulated from one another and connected by a bridge wire (not shown). The bridge wire is preferably embedded in one or more layers of
5 pyrotechnic compositions designed to give a flash (heat) of sufficient intensity to ignite the booster composition.

The exemplary gas generating device 20 comprises a first housing member 21, a second housing member 22,
10 and a choke plate 23 interposed between the first and second housing members. The first housing member 21 has a flange 30 which is bent over to secure the choke plate and the second housing member to the first housing member. The housing members and choke plate
15 may be formed of any suitable material, preferably aluminum or steel.

The first housing member 21 is cup shaped with a recess 36 extending inwardly from the closed end thereof. As used herein terms such as "inward",
20 "inwardly" and so forth are understood to refer to directions going toward the interior of the gas generating device, and terms such as "outward" and "outwardly" are understood to refer to directions going toward the exterior of the gas generating
25 device. The recess 36 in the closed end of the first housing member 21 has an aperture 35 therethrough to accommodate the assembly of a squib 24 with the first housing member. The squib is secured in place by a collar 25 which is telescoped over the inside surface
30 of the closed end of the first housing member. A cup 27 containing a booster composition 26 is telescoped over the outside surface of the collar 25. The gas generating composition 28 is located in the first housing member 21.

In accordance with the present invention an auto-ignition material 33 is disposed within the housing 21 in close proximity to the gas generating composition 28. A choke plate 23 having a plurality of apertures 29 therethrough is located at the open end of the first housing member 21. A second housing member 22 is located at the open end of the first housing member 21 with the choke plate 23 located between the first and second housing members. The second housing member 22 has a plurality of apertures 32 therethrough. The second housing member is cup shaped. A flange 31 is located at the open end of the second housing member. In this exemplary device the choke plate 23 and the flange 31 of the second housing member are secured to the first housing member by a flange 30 of the first housing member 21 which is bent over inwardly. Element 37 is a recess in the center of the annular ring of the second housing member 22 which has a plurality of apertures 32 therethrough.

Referring next to Fig. 3 there is shown an enlarged fragmentary view of an alternative embodiment of the autoignition system of the present invention. In this embodiment a coating 40 of material such as an acrylate or silicone overlies the autoignition material 33 to protect it from being abraded by the gas generating material 28.

Referring next to Fig. 4 there is shown an enlarged fragmentary view of an alternative embodiment of the autoignition system of the present invention. In this embodiment a barrier layer 41 of material such as an acrylate or silicone is disposed between the autoignition material 33 and the aluminum housing 21 to protect the housing from being corroded by the $\text{Pb}(\text{SCN})_2$ in the coating autoignition composition.

Referring next to Fig. 5 there is shown an enlarged fragmentary view of another alternative embodiment of the autoignition system of the present invention. In this embodiment a barrier layer 42 of an acrylate or silicone is disposed between the autoignition composition and the housing 21 to protect the housing from being corroded by the $\text{Pb}(\text{SCN})_2$ in the autoignition composition and a coating 43 of an acrylate or silicone the autoignition composition 33 to protect it from being abraded by the gas generating material 28 and to prevent absorption of water.

CLAIMS:

1. An autoignition composition for application to the interior of a gas generating device housing comprising:

- 5 a) lead thiocyanate; and
 b) a chlorate.

2. An autoignition composition according to claim 1 which additionally comprises at least one
10 material selected from binders and flow agents/thickeners.

3. An autoignition composition according to claim 1 wherein the chlorate is selected from the
15 group consisting of sodium chlorate, potassium chlorate, barium chlorate and mixtures thereof.

4. An autoignition composition according to claim 3 which additionally comprises at least one
20 element selected from water soluble binders and hydrophilic flow agent/thickeners.

5. An autoignition composition according to claim 4 wherein said composition
25 comprises, based on % dry weight:

lead thiocyanate	25-50%
potassium chlorate	25-50%
water soluble binder	0-5%
hydrophilic flow agent/thickener	0-5%.

6. An autoignition composition according to claim
4 which comprises:

- a) lead thiocyanate;
- b) a chlorate selected from the group
5 consisting of sodium chlorate, potassium
chlorate, barium chlorate and mixtures
thereof;
- c) a binder at a concentration of from 0-5% by
dry weight; and
- 10 d) a flow agent/thickener at a concentration of
from 0-5% by dry weight.

7. An autoignition composition according to
claim 6 wherein the binder is selected from the group
15 consisting of hydrated lime, sodium silicate,
carboxymethylcellulose, natural rubber, synthetic
rubber, resins, lacquers, nitrocellulose,
ethylcellulose, polyamides, polyurethanes, epoxy
compounds, starch, dextrans, lignin, polyvinyl
20 alcohol, resorcinol formaldehyde, phenol formaldehyde
and polyvinyl ethers.

8. An autoignition composition according to
claim 6 wherein the binder is water soluble.

25 9. An autoignition composition according to
claim 6 wherein the flow agent/thickener is selected
from the group consisting of hydrophilic silicas.

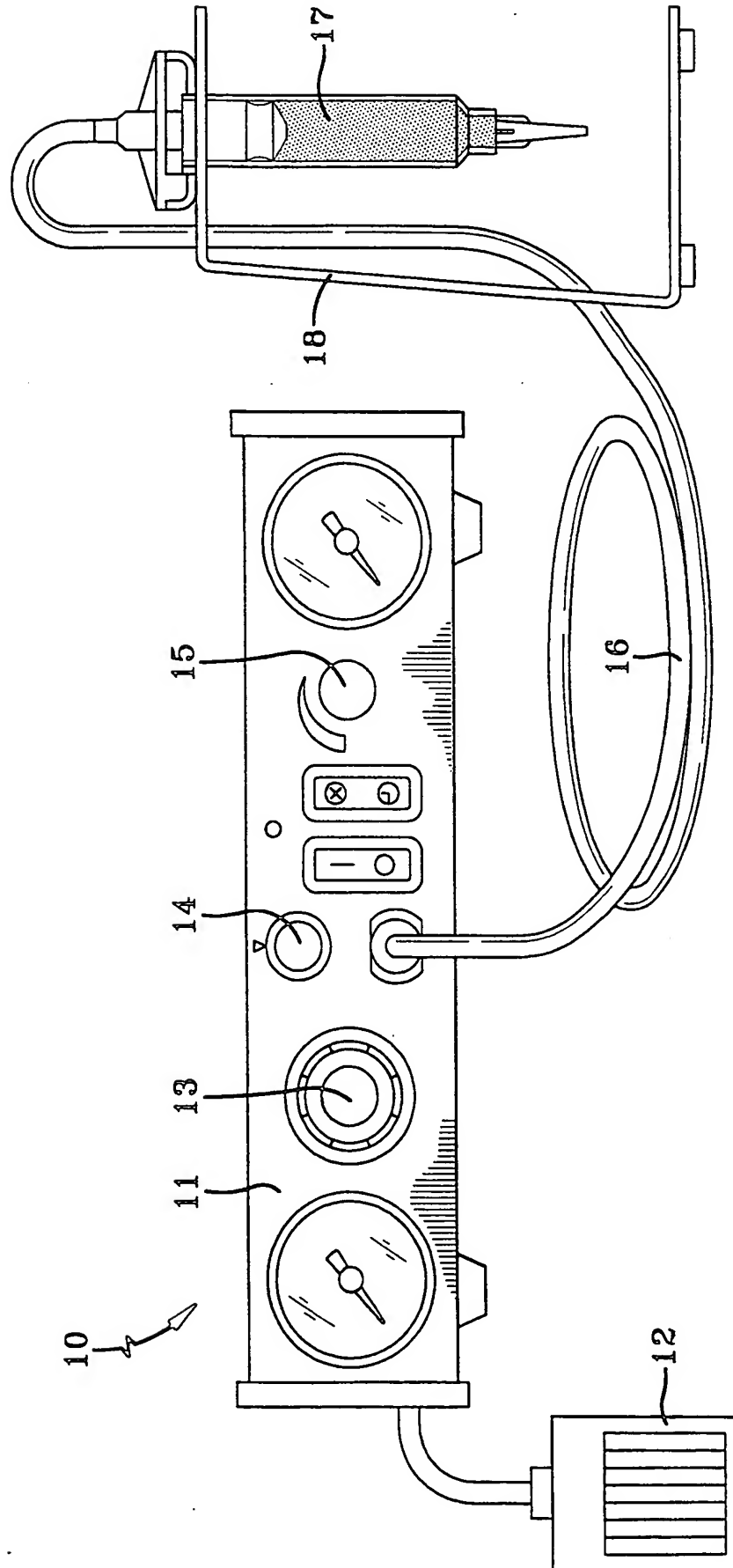


FIG-1

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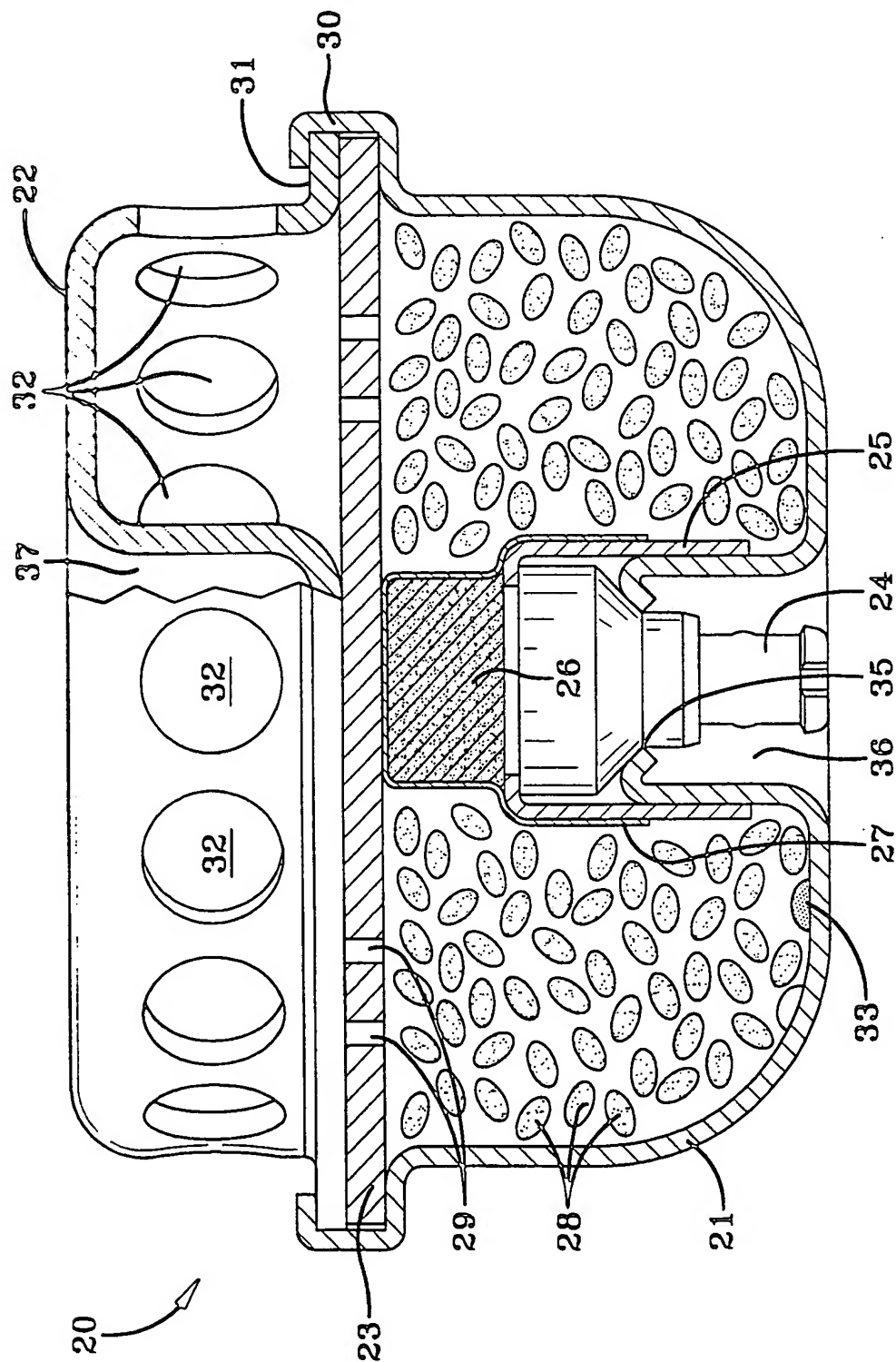
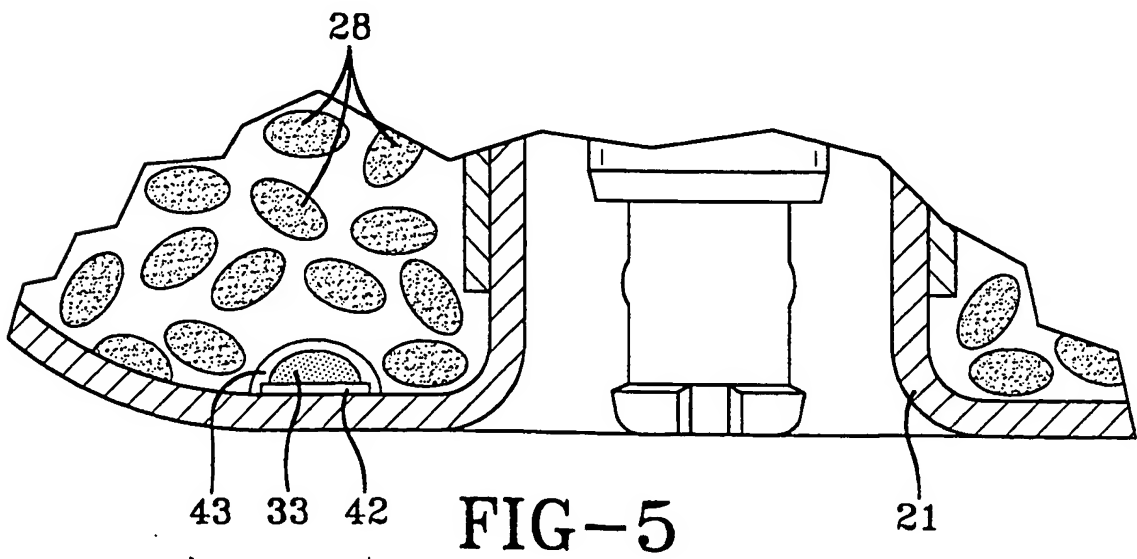
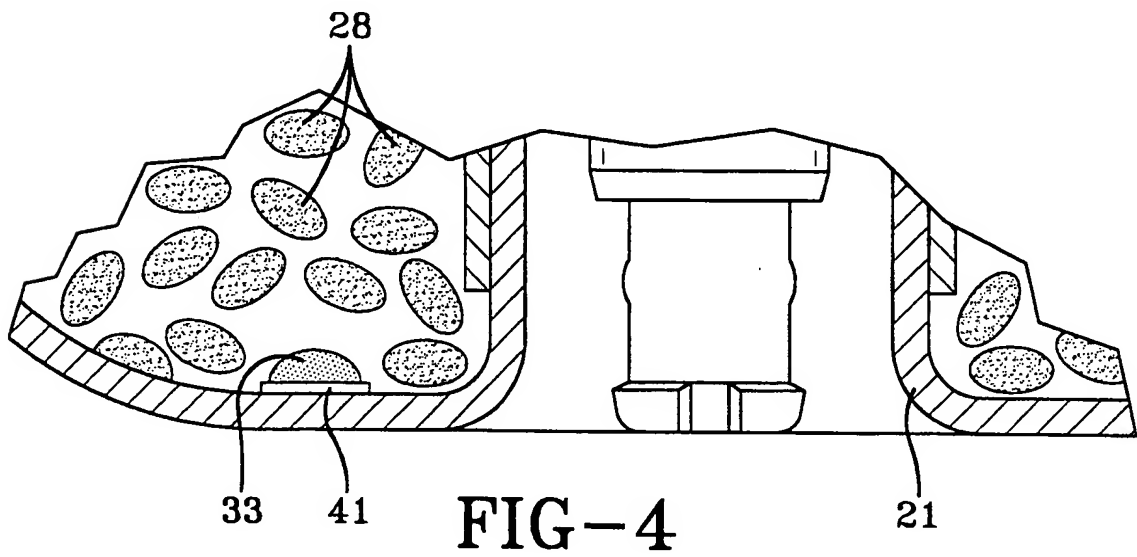
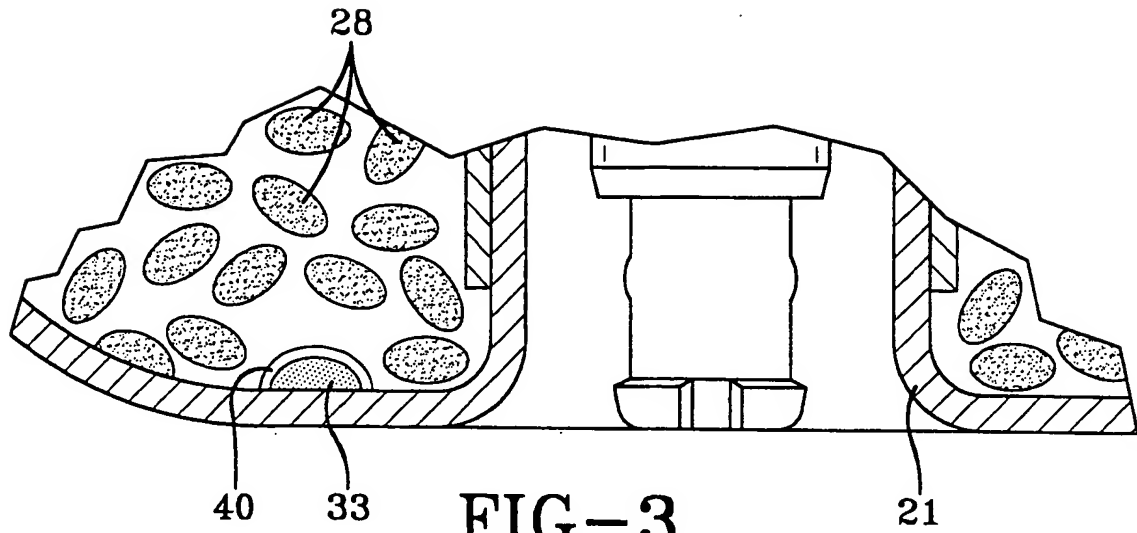


FIG-2

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INTERNATIONAL SEARCH REPORT

International application No.

PCT/US97/17329

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :C06B 29/02

US CL :149/77

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 149/77

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X -- Y	US 5,557,061 A (RAMASWAMY) 17 September 1996, col. 4, lines 18-28.	1-4, 7-10 ----- 1-5, 7-10
Y	US 4,994,125 A (MEI) 19 February 1991, the Abstract, col. 6, lines 1-5.	1-5, 7-10
X -- Y	US 5,019,192 A (RAMASWAMY) 28 May 1991, col. 2, lines 20-24.	1-4, 7-10 ----- 1-5, 7-10
X -- Y	US 4,566,921 A (DUGUET) 28 January 1986, col. 4, lines 15-19.	1-5, 7-10 ----- 1-5, 7-10
Y	US 1,189,238 A (CALVET) 04 July 1916, page 1, lines 59-60 and	1-5, 7-10



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
A document defining the general state of the art which is not considered to be of particular relevance	*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*A* document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means	
P document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

19 JANUARY 1998

Date of mailing of the international search report

06 MAR 1998

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